



## Fabrication of nanopowders by high energy ball milling and low temperature sintering of $\text{Mg}_2\text{SiO}_4$ microwave dielectrics

Lin Cheng<sup>a,\*</sup>, Peng Liu<sup>a</sup>, XiaoMing Chen<sup>a</sup>, WenCheng Niu<sup>a</sup>, GuoGuang Yao<sup>a</sup>, Cheng Liu<sup>a</sup>, XiaoGang Zhao<sup>a</sup>, Qian Liu<sup>a</sup>, HuaiWu Zhang<sup>b</sup>

<sup>a</sup> College of Physics and Information Technology, Shaanxi Normal University, Xi'an 710062, China

<sup>b</sup> The Key Laboratory of Electronic Thin Film and Integrated Device, University of Electronic Science and Technology of China, Chengdu 610054, China

### ARTICLE INFO

#### Article history:

Received 19 May 2011

Received in revised form 15 October 2011

Accepted 18 October 2011

Available online 25 October 2011

#### Keywords:

Mechanical alloying

Nanostructured materials

Ceramics

X-ray diffraction

### ABSTRACT

$\text{Mg}_2\text{SiO}_4$  nanopowders were prepared from MgO and  $\text{SiO}_2$  mixtures by using a high energy ball milling method, combined with subsequent calcination at low temperatures. After milling for 30 h, pure phase  $\text{Mg}_2\text{SiO}_4$  nanopowders with an average grain size of 147.4 nm were obtained at 850 °C, 300 °C lower than that required by a conventional solid state reaction process.  $\text{Mg}_2\text{SiO}_4$  ceramics sintered at a low temperature of 1075 °C showed almost full density and excellent microwave dielectric properties ( $\epsilon_r = 7.2$ ,  $Q \times f = 193,800$  GHz,  $\tau_f = -58$  ppm/°C).

© 2011 Elsevier B.V. All rights reserved.

### 1. Introduction

Recently, much attention has been paid to the development of microwave telecommunication technologies because of the increased requirements for microwave applications. These applications demand microwave substrate materials with high quality factor ( $Q \times f$ ) to achieve high selectivity, low dielectric constant ( $\epsilon_r$ ) to reduce the delay time of electronic signal, and nearly zero temperature coefficient of resonant frequency ( $\tau_f$ ) for frequency stability. Promising candidates include as  $\text{Mg}_2\text{SiO}_4$  ( $Q \times f = 40,000\text{--}240,000$  GHz,  $\epsilon_r = 6\text{--}7$ ,  $\tau_f = -60$  ppm/°C) [1,2],  $\text{Al}_2\text{O}_3$  ( $Q \times f = 680,000$  GHz,  $\epsilon_r = 10$ ,  $\tau_f = -55$  ppm/°C) [3,19],  $\text{Mg}_2\text{SnO}_4$  ( $Q \times f = 55,100$  GHz,  $\epsilon_r = 8.41$ ,  $\tau_f = -62$  ppm/°C) [11],  $\text{Ba}(\text{Zn}_{1/3}\text{Ta}_{2/3})\text{O}_3$  ( $Q \times f = 120$  THz) [23],  $\text{Li}_2\text{MgTi}_3\text{O}_8$  ( $Q \times f = 36,200$  GHz,  $\epsilon_r = 26$ ,  $\tau_f = -2$  ppm/°C) [24] and other microwave dielectrics materials [25–33]. Among these materials, forsterite  $\text{Mg}_2\text{SiO}_4$  has attracted a great attention with low dielectric constant and loss tangent.

In MgO– $\text{SiO}_2$  binary systems, there are  $\text{Mg}_2\text{SiO}_4$  and  $\text{MgSiO}_3$  phases. A number of methods to synthesize  $\text{Mg}_2\text{SiO}_4$  powders, such as solid state reaction, sol–gel, and aqueous methods [1,5,6,10,14,17]. Usually, with a solid state reaction method for preparation of  $\text{Mg}_2\text{SiO}_4$  ceramics,  $\text{MgSiO}_3$  as a secondary phase

is almost inevitable, a major cause of serious damage to the microwave dielectric properties of  $\text{Mg}_2\text{SiO}_4$  ceramics. Various efforts have been employed to synthesize single  $\text{Mg}_2\text{SiO}_4$  phase such as sol–gel and other chemical methods [5,12]. By introducing nonstoichiometry and adjusting the Mg/Si ratios, Song et al. obtained pure phase  $\text{Mg}_2\text{SiO}_4$  ceramics with an enhanced  $Q \times f$  value (114,730 GHz), but the sintering temperature of the ceramics was as high as 1350 °C [7]. How to obtain pure  $\text{Mg}_2\text{SiO}_4$  phase and sintering the ceramics at low sintering temperatures is still a challenging issue.

High energy ball milling (HEBM) is a simple and efficient method for preparing nanometer powders and HEBM of starting powder is effective to enhance the sintering kinetics [13]. This is because they have nanometer particle size and very high homogeneity, leading to a reduced phase formation temperature [8]. Furthermore, compared with soft chemical methods [5], HEBM is suitable for mass production. In this study, we prepared  $\text{Mg}_2\text{SiO}_4$  powders via HEBM method. Single phase  $\text{Mg}_2\text{SiO}_4$  ceramics were obtained at lower temperatures from the HEBM derived mixtures. The effects of HEBM on phase transformation, sintering behavior, and microwave dielectric properties of the  $\text{Mg}_2\text{SiO}_4$  ceramics were reported.

### 2. Experimental procedures

Commercially available MgO (99.99% purity) and  $\text{SiO}_2$  (99.99% purity) powders were used as the starting materials with the nominal composition of  $\text{Mg}_2\text{SiO}_4$ . The mixtures were milled for 5–30 h with a Fritsch Vario-Planetary HEBM system in air. Tungsten carbide vial with diameter of 80 mm and tungsten carbide balls with diameter of 10 mm were used as milling medium. The rotational speed of vials and

\* Corresponding author.

E-mail address: [chenglin@stu.snnu.edu.cn](mailto:chenglin@stu.snnu.edu.cn) (L. Cheng).

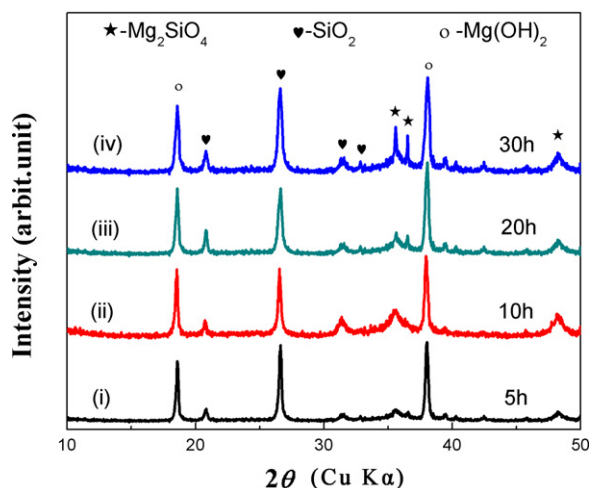


Fig. 1. XRD patterns of the MgO–SiO<sub>2</sub> mixtures milled for different times.

ball-to-powder-to-deionized water mass ratio were 300 rpm and 20:1:1.5, respectively. After drying, the milled powders were calcined at 500–900 °C for 3 h at 3 °C/min in air. The calcined powders were milled again for 10 h. After drying, the powders mixed with 5 wt.% PVA as binder and granulated. The granulated powders were pressed into pellets with cylindrical shape under the pressure of 170 MPa and sintered at 1000–1100 °C for 3 h in air.

Reaction behaviors of the milled powders were investigated by using thermal gravimetric and differential thermal analysis (TG/DTA) (SDT Q600 V8.0 Build 95, American) with heating rate of 10 °C/min in air from room temperature to 1100 °C. Phase constituents of the samples were characterized by using X-ray diffraction (XRD) (Rigaku D/max 2250, Japan) (40 kV, 50 mA) with Cu K<sub>α</sub> radiation. Microstructures and grain size of the powders and ceramics were examined by using scanning electron microscopy (SEM) (Quanta 200, Germany) and a laser particle size analyzer (BI-90Plus, America), respectively. Densities of the ceramics were measured by using the Archimedes methods. Dielectric behaviors at microwave frequency were measured by the TE<sub>018</sub> shielded cavity method with a network analyzer (8720ES, Agilent, USA) and a temperature chamber (Delta Design 9023, USA). The  $\tau_f$  value was calculated by the following formula [20]:

$$\tau_f = \frac{f_{60} - f_{20}}{f_{60}(60 - 20)} \times 10^6 (\text{ppm}/^\circ\text{C}) \quad (1)$$

where  $f_{60}$  and  $f_{20}$  were the TE<sub>018</sub> resonant frequencies at 60 and 20 °C, respectively.

### 3. Results and discussion

Fig. 1 shows XRD patterns of the powders milled for different times. After milling for 5 h, MgO disappeared and Mg(OH)<sub>2</sub> was detected (chemical reaction between MgO and hot water (150–200 °C)) [18]. With increasing milling time, forsterite Mg<sub>2</sub>SiO<sub>4</sub> phase content with relatively weak diffraction intensity increases. As the milling time was increased to 30 h, two strongest peaks of Mg<sub>2</sub>SiO<sub>4</sub> phase were obviously detected. Hence, Mg<sub>2</sub>SiO<sub>4</sub> forsterite could be formed by mechanochemical reaction, even though the pure phase could not be synthesized by HEBM alone.

Fig. 2 shows TG/DTA curves of the powders milled for 30 h. The DTA curve exhibits one endothermic peak starting at 270 °C, which is accompanied by a weight loss of approximately 0.8% due to the decomposition of Mg(OH)<sub>2</sub> [15]. The exothermic peak starting at 570 °C is related to the formation of forsterite phase, so calcination temperatures were determined to be higher than 570 °C [16].

Fig. 3 shows XRD patterns of the 30 h HEBM powders and those being calcined at various temperatures for 3 h. As shown in Fig. 3(i) for the uncalcined powders, the main diffraction peaks are attributed to SiO<sub>2</sub> and Mg(OH)<sub>2</sub> with Mg<sub>2</sub>SiO<sub>4</sub> as a minor phase. Calcined at 600 °C (Fig. 3(ii)), the peak intensity of Mg<sub>2</sub>SiO<sub>4</sub> is obviously enhanced, in agreement with the DTA analysis shown in Fig. 2. Further increasing calcined temperatures, forsterite Mg<sub>2</sub>SiO<sub>4</sub> phase content increases with a disappearance of SiO<sub>2</sub> and Mg(OH)<sub>2</sub> phases. As the calcining temperature is increased up to 850 °C

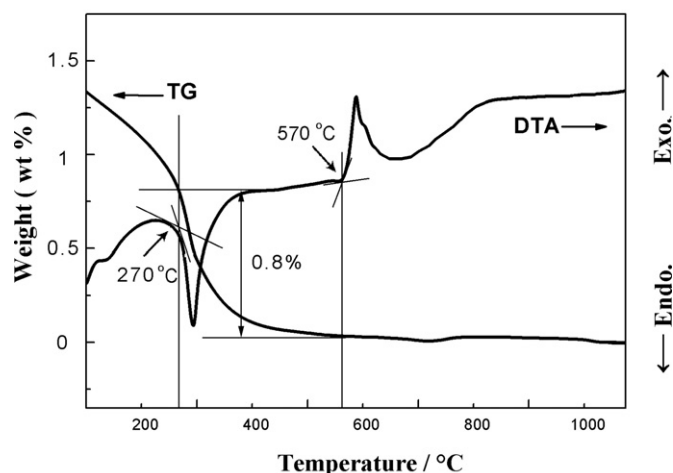


Fig. 2. TG/DTA curves of the MgO–SiO<sub>2</sub> mixtures milled for 30 h.

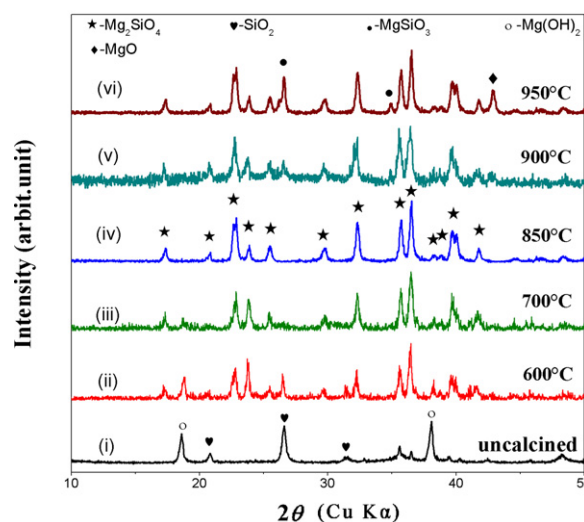


Fig. 3. XRD patterns of the MgO–SiO<sub>2</sub> mixtures milled for 30 h and calcined at different temperatures for 3 h.

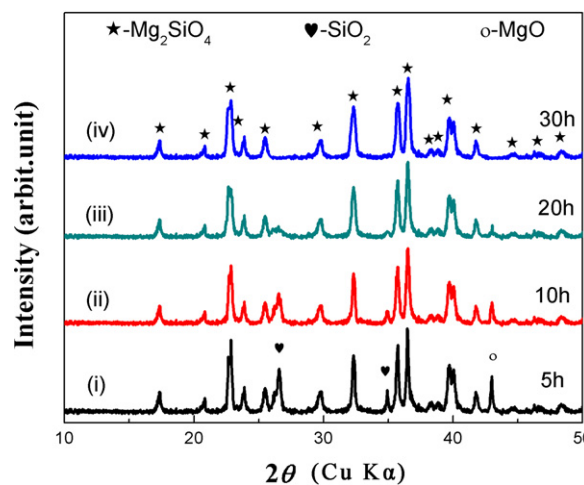
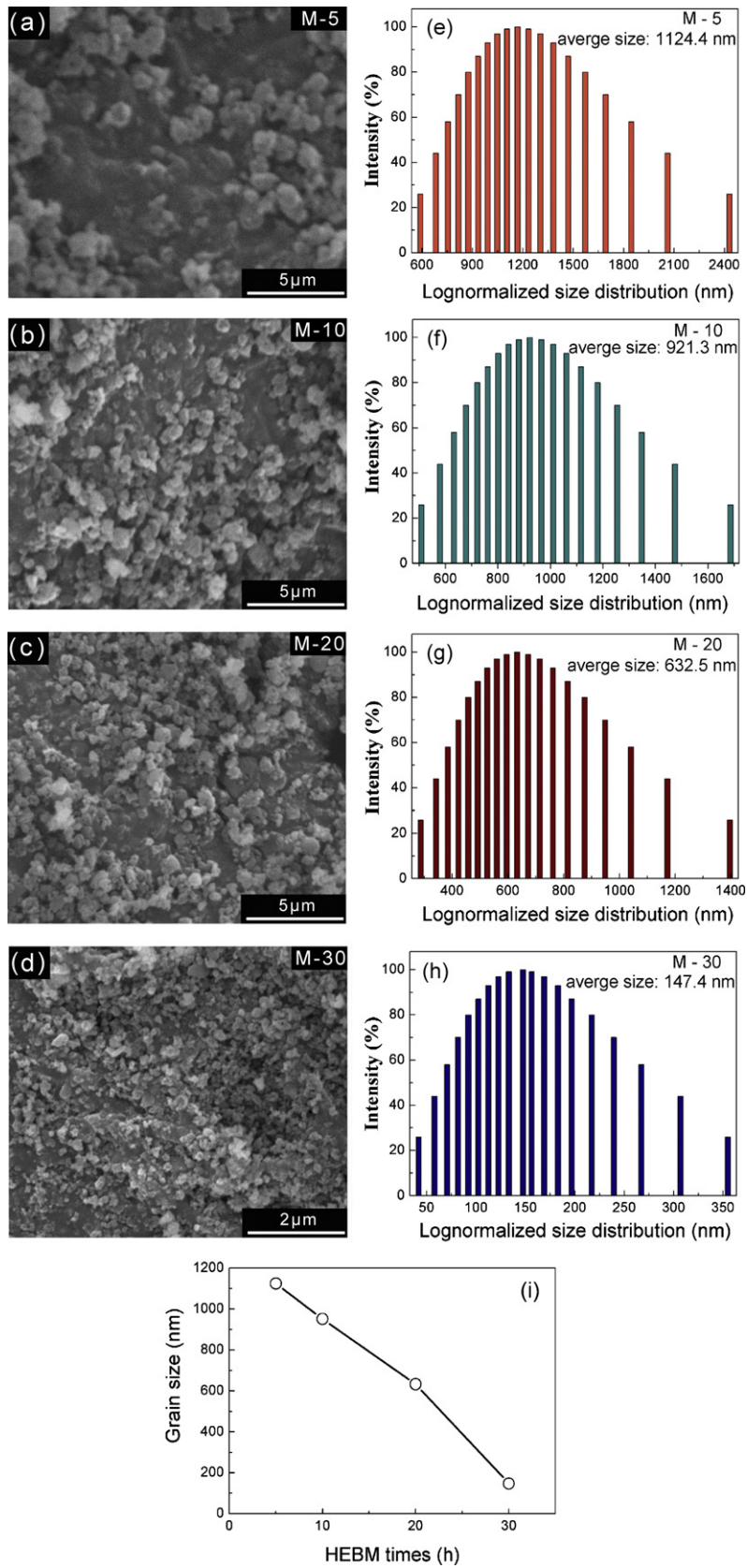


Fig. 4. XRD patterns of the MgO–SiO<sub>2</sub> mixtures milled for different times and calcined at 850 °C for 3 h.



**Fig. 5.** Representative SEM micrographs (a–d), particle size distribution of the MgO and SiO<sub>2</sub> mixtures calcined at 850 °C for 3 h (e–h), average particle size as a function of milling times (i).

(Fig. 3(iv)), a pure phase forsterite is obtained. However, calcination above 900 °C resulted in the appearance of  $\text{MgSiO}_3$  and  $\text{MgO}$  phases (Fig. 3(v and vi)), related to the decomposition of  $\text{Mg}_2\text{SiO}_4$  at elevated temperatures [21]. Hence XRD analysis indicated that the  $\text{Mg}_2\text{SiO}_4$  purity forsterite phase is obtained by mechanochemical reaction using HEBM for 30 h and calcined at 850 °C which is 300 °C lower than that required by a conventional solid state reaction technique [2,7]. Therefore, calcination temperature of forsterite  $\text{Mg}_2\text{SiO}_4$  was determined as 850 °C.

Fig. 4 shows XRD patterns of the powders milling at different times, and calcined at 850 °C dwelling for 3 h. For the calcined powders milled for 5 h (Fig. 4(ii)),  $\text{Mg}_2\text{SiO}_4$  appears as dominant phase with  $\text{SiO}_2$  and  $\text{MgO}$  as minor phases [18]. As the milling time was increased to 30 h (Fig. 4(iv)), a single phase  $\text{Mg}_2\text{SiO}_4$  with a well-developed XRD pattern is obtained. Therefore, HEBM is an effective approach to reduce the phase formation temperature of  $\text{Mg}_2\text{SiO}_4$  phase [8], meanwhile increasing milling time is beneficial for obtaining the pure  $\text{Mg}_2\text{SiO}_4$  phase.

Fig. 5 shows representative SEM micrographs (Fig. 5(a–d)) and particle size distribution of the  $\text{MgO}$  and  $\text{SiO}_2$  mixtures calcined at 850 °C for 3 h (Fig. 5(e–h)) and average particle size as a function of different milling times (Fig. 5(i)). As shown in Fig. 5(i), particle size decreases with increasing milling time. Compared with the conventional ball milling method, HEBM leads to a reduced average particle size and a narrowed size distribution [9,22]. Similar result was ever reported for various ferroelectric compounds and alloys [8]. For the powders calcined at 850 °C as the HEBM time increasing

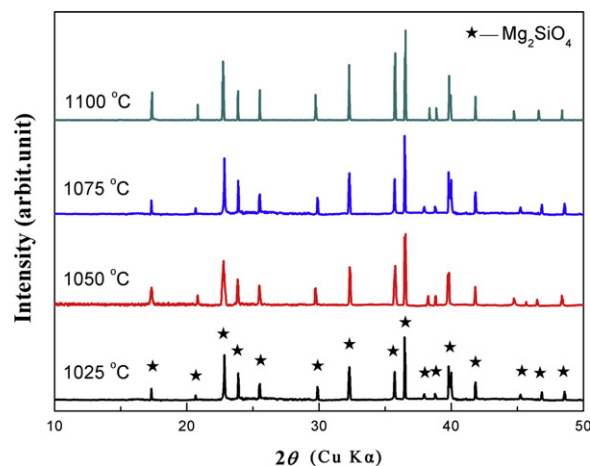


Fig. 6. XRD patterns of the  $\text{Mg}_2\text{SiO}_4$  ceramics sintered at 1025–1100 °C.

from 5 h to 30 h, the average particle size is reduced gradually from 1124.4 (Fig. 5(e)) to 147.4 nm (Fig. 5(h)), in agreement with the SEM micrographs shown in Fig. 5(a–d). Particle size of powders milled for 30 h calcined at 850 °C is 120–150 nm (Fig. 5(d) and (h)). Therefore, the  $\text{MgO}$ – $\text{SiO}_2$  mixtures milled 30 h and calcined at 850 °C was employed to fabricate  $\text{Mg}_2\text{SiO}_4$  ceramics.

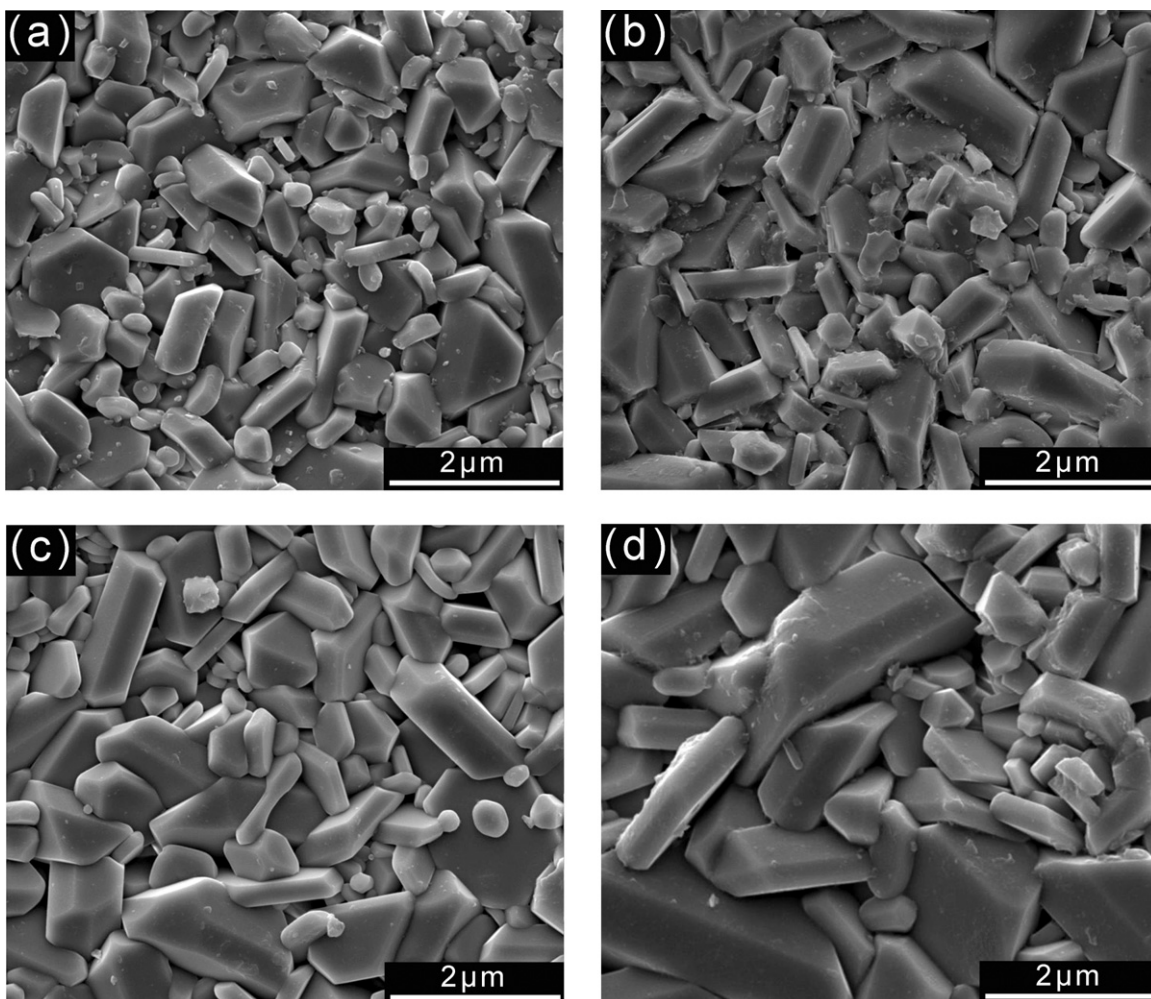


Fig. 7. SEM surface microstructures of the forsterite ceramics sintered at (a) 1025 °C, (b) 1050 °C, (c) 1075 °C, and (d) 1100 °C for 3 h in air.

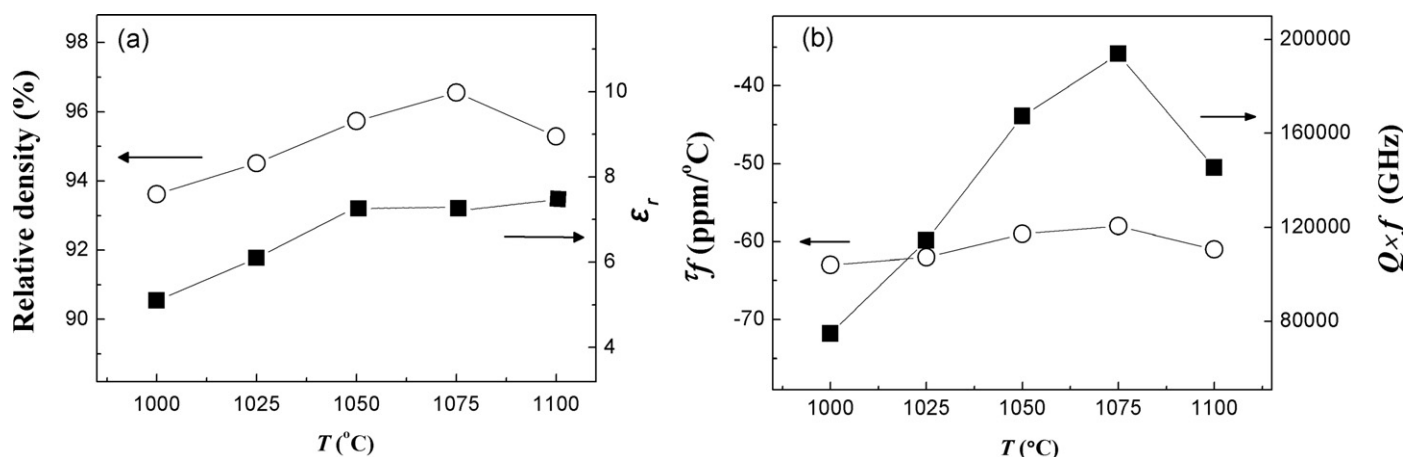


Fig. 8. (a) Relative density, dielectric constant ( $\epsilon_r$ ), (b) quality factor ( $Q \times f$ ) and  $\tau_f$  of the Mg<sub>2</sub>SiO<sub>4</sub> ceramics as a function of sintering temperatures.

Fig. 6 shows XRD patterns of the Mg<sub>2</sub>SiO<sub>4</sub> ceramics sintered at 1025 °C to 1100 °C. As shown in Fig. 6, all the ceramics sintered at 1025–1100 °C are to be a single Mg<sub>2</sub>SiO<sub>4</sub> phase. Fig. 7 shows SEM surface microstructures of the Mg<sub>2</sub>SiO<sub>4</sub> ceramics as-sintered at 1025–1100 °C. All samples have dense microstructures, but for sample sintered at 1100 °C an abnormal growth of grain size was appeared (Fig. 7(d)), which will make a decrease of  $Q \times f$  values. Fig. 8(a) shows relative density and dielectric constant ( $\epsilon_r$ ) of the Mg<sub>2</sub>SiO<sub>4</sub> ceramics from the 30 h milled powders sintered at different temperatures. The relative densities increase to their maximum values as the sintering temperatures increase from 1000 °C to 1075 °C, and then decrease slightly with further increasing temperatures to 1100 °C, due to the abnormal grain growth shown in Fig. 7(d). The optimum sintering temperature (1075 °C) is much (300 °C) lower than other's works reported in recent years [1,7]. Relative density of the sample sintered at 1075 °C reaches to 96.56%, same level comparing with previous reports of the materials prepared by the other methods [4]. With increasing sintering temperatures from 1000 to 1075 °C,  $\epsilon_r$  values increased from 5.8 to 7.2 due to the increased relative density. Quality factor ( $Q \times f$ ) values exhibit a similar trend with relative density of the samples as a function of sintering temperatures (Fig. 8(b)). The  $Q \times f$  values increase with the growth grain size, but as the sintering temperature increasing up to 1100 °C the abnormal grain growth makes the  $Q \times f$  values decrease. With increasing temperatures from 1000 to 1075 °C, the  $\tau_f$  values vary from -63 to -58 ppm/°C and the  $Q \times f$  values increase from 74,800 to 193,800 GHz. The optimum  $Q \times f$  value (193,800 GHz) is comparable with those achieved by a conventional solid state reaction method sintered at 1350–1550 °C [2,7].

#### 4. Conclusions

The phase formation temperature of Mg<sub>2</sub>SiO<sub>4</sub> nanopowders from MgO and SiO<sub>2</sub> was reduced about 300 °C by using HEBM. The lowered forsterite Mg<sub>2</sub>SiO<sub>4</sub> phase formation temperature was attributed to the refinement of the oxides and mechanical alloying process. Mg<sub>2</sub>SiO<sub>4</sub> powders with an average grain size of 147.4 nm were obtained by HEBM for 30 h and calcined at 850 °C for 3 h, 300 °C lower than required by a conventional solid state reaction method. The forsterite Mg<sub>2</sub>SiO<sub>4</sub> ceramics from HEBM powders sintered at 1075 °C showed dense microstructures and excellent microwave dielectric properties ( $\epsilon_r = 7.2$ ,  $Q \times f = 193,800$  GHz,  $\tau_f = -58$  ppm/°C). It is believed that the HEBM technique can be extended to other microwave dielectric materials.

#### Acknowledgement

The work was supported by the National Natural Science Foundation of China (Grants Nos. 51072110 and 51132003).

#### References

- [1] T. Sugiyama, T. Tsunooka, K. Kakimoto, H. Ohsato, J. Eur. Ceram. Soc. 26 (2006) 2097–2100.
- [2] T. Tsunooka, M. Androu, Y. Higashida, H. Sugiura, H. Ohsato, J. Eur. Ceram. Soc. 23 (2003) 2573–2578.
- [3] A. Stiegeschmitt, A. Roosen, C. Ziegler, S. Martius, L. Schmidt, J. Eur. Ceram. Soc. 24 (2004) 1463–1466.
- [4] S. Ni, L. Chou, J. Chang, Ceram. Int. 33 (2007) 83–88.
- [5] K.P. Sanosh, A. Balakrishnan, L. Francis, T.N. Kim, J. Alloys Compd. 495 (2011) 113–115.
- [6] F. Tavangarian, R. Emadi, Mater. Lett. 65 (2011) 126–129.
- [7] K.X. Song, X.M. Chen, X.C. Fan, J. Am. Ceram. Soc. 90 (2007) 1808–1811.
- [8] L.B. Kong, T.S. Zhang, J. Ma, F. Boey, Prog. Mater. Sci. 53 (2008) 207–322.
- [9] Z.F. Fu, P. Liu, X.M. Chen, J.L. Ma, H.W. Zhang, J. Alloys Compd. 493 (2010) 441–444.
- [10] S.C. Prashantha, B.N. Lakshminarasappa, B.M. Nagabhushana, J. Alloys Compd. 509 (2011) 10185–10189.
- [11] Y.C. Chen, Y.N. Wang, C.H. Hsu, J. Alloys Compd. 509 (2011) 9650–9653.
- [12] M. Kharaziha, M.H. Fathi, Ceram. Int. 35 (2009) 2449–2454.
- [13] S.B. Kim, S.J. Kim, C.H. Kim, W.S. Kim, K.W. Park, Mater. Lett. 65 (2011) 3313–3316.
- [14] S. Sano, N. Saito, S. Matsuda, N. Ohashi, H. Haneda, J. Am. Ceram. Soc. 89 (2006) 568–574.
- [15] D. Goeriot, J.C. Dubois, D. Merle, F. Thevenot, P. Exbrayat, J. Eur. Ceram. Soc. 18 (1998) 2045–2056.
- [16] A. Saberi, B. Alinejad, Z. Negahdari, F. Kazemi, A. Almasi, Mater. Res. Bull. 42 (2007) 666–673.
- [17] M.F. Zawrah, Mater. Sci. Eng. A 382 (2004) 362–370.
- [18] W.F. Giauque, Contribution from the chemical laboratory of the university of california 71 (1949) 3192.
- [19] H. Ohsato, T. Tsunooka, Y. Ohishi, Y. Miyauchi, M. Ando, K. Kakimoto, J. Korean Ceram. Soc. 40 (2003) 350–353.
- [20] B.W. Hakki, P.D. Coleman, IRE Trans. Microwave Theory & Tech. MTT-8 (1960) 402–410.
- [21] I.H. Jung, S.A. Deckerov, A.D. Pelton, J. Eur. Ceram. Soc. 25 (2005) 313–333.
- [22] L.B. Kong, T.S. Zhang, J. Ma, F. Boey, J. Eur. Ceram. Soc. 23 (2003) 2247–2256.
- [23] L. Nedelcu, M.I. Toacsan, M.G. Banciu, A. Ioachim, J. Alloys Compd. 509 (2011) 477–481.
- [24] X. Chen, H. Zhou, L. Fang, X. Liu, Y. Wang, J. Alloys Compd. 509 (2011) 5829–5832.
- [25] M. He, Sh. Zhang, X. Zhou, B. Li, J. Wan, J. Alloys Compd. 509 (2011) 4260–4263.
- [26] Y.B. Chen, J. Alloys Compd. 509 (2011) 2285–2288.
- [27] J. Guo, D. Zhou, H. Wang, X. Yao, J. Alloys Compd. 509 (2011) 5863–5865.
- [28] Z. Liang, L.L. Yuan, J.J. Bian, J. Alloys Compd. 509 (2011) 1893–1896.
- [29] M.A. Sanoj, C.P. Reshmi, K.P. Sreena, M.R. Varma, J. Alloys Compd. 509 (2011) 3089–3095.
- [30] L. Fang, D. Chu, H. Zhou, X. Chen, Z. Yang, J. Alloys Compd. 509 (2011) 1880–1884.
- [31] A. Surjith, N.K. James, R. Ratheesh, J. Alloys Compd. 509 (2011) 9992–9995.
- [32] M.K. Suresh, A. John, J.K. Thomas, P.R.S. Wariar, S. Solomon, J. Alloys Compd. 509 (2011) 2401–2406.
- [33] S. Wu, J. Luo, J. Alloys Compd. 509 (2011) 8126–8129.